

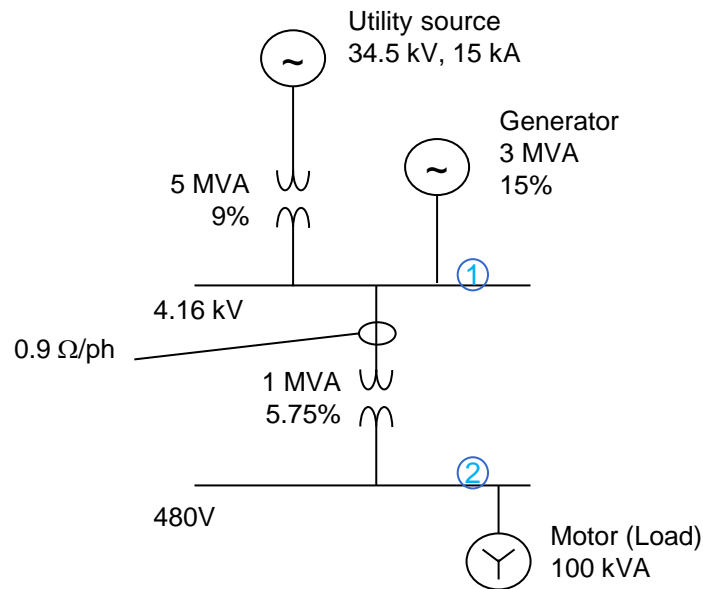
Power System Analysis:

Load Flow / Power Factor

Dave Loucks, PhD, PE, CEM

Load Flow

- What is the nominal voltage
 - At bus ① ?
 - At bus ② ?
- ... assuming only load is 100 kVA motor?

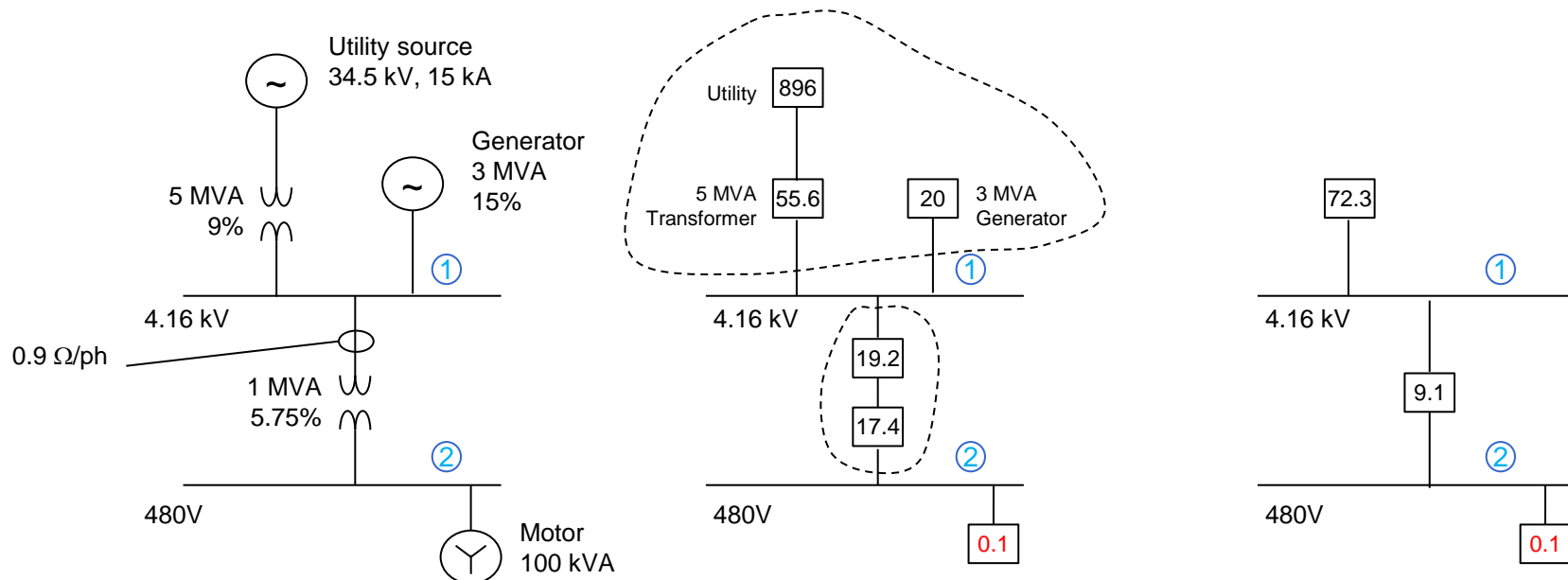


Load Flow

- Convert all components to equivalent MVA
 - $MVA = \sqrt{3} \cdot kV \cdot kA$ (use for incoming)
 - $MVA = kV^2 / Z$ (use for cables)
 - $MVA = MVA / \%Z$ (use for transformers, gens, motors)

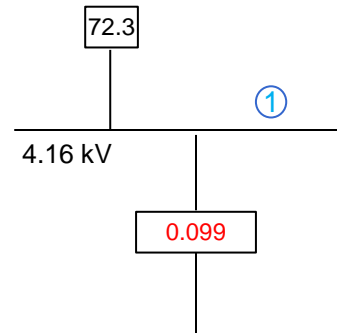
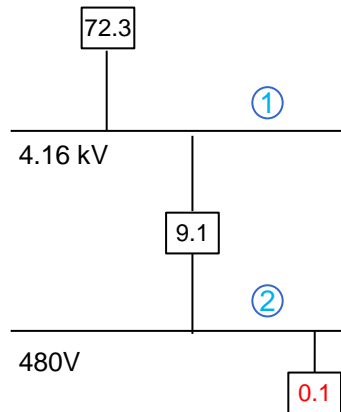
Converted to MVA

- Same procedure as discussed yesterday
 - Except motors are shown at nominal not SC MVA



Calculate Bus 1 Voltage

- Voltage on bus 1



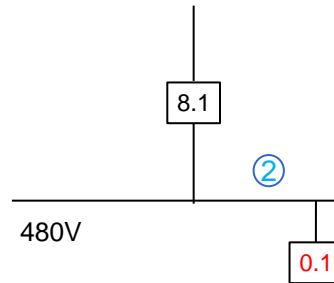
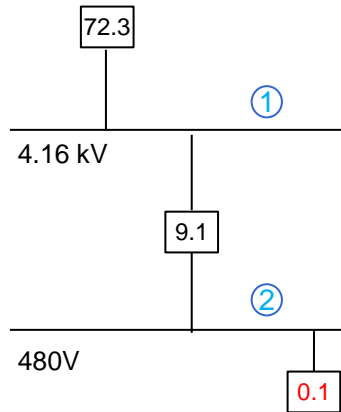
- Voltage drop is $\Delta\%$ of MVA values

$$\frac{72.3 - 0.099}{72.3} = 99.86\%$$



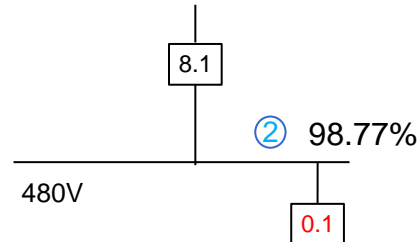
Calculate Bus 2 Voltage

- Voltage on bus 2



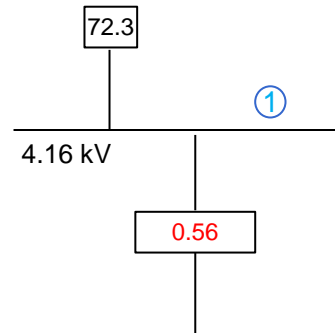
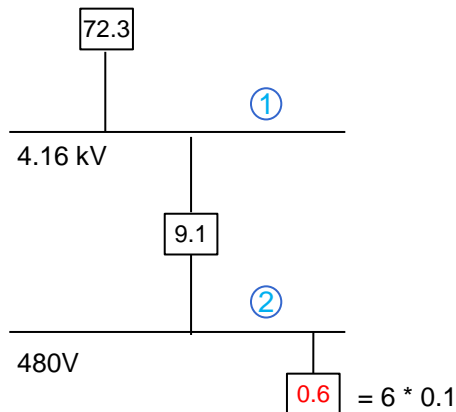
- Voltage drop is $\Delta\%$ of MVA values

$$\frac{8.1 - 0.1}{8.1} = 98.77\%$$



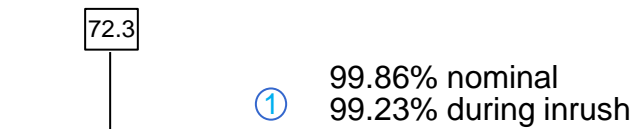
Calculate Bus 1 Voltage During Inrush

- Voltage on bus 1 (assume 6x locked rotor)



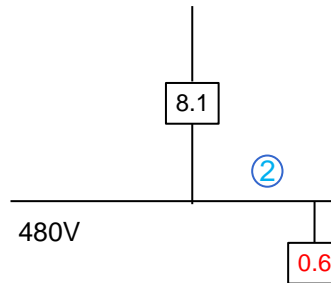
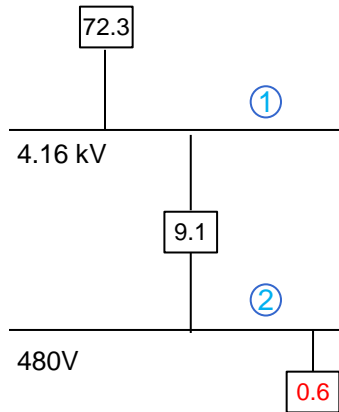
- Voltage drop is $\Delta\%$ of MVA values

$$\frac{72.3 - 0.56}{72.3} = 99.23\%$$



Calculate Bus 2 Voltage During Inrush

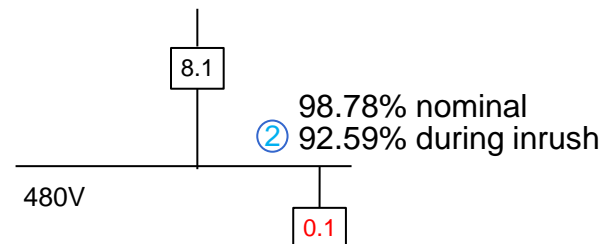
- Voltage on bus 2



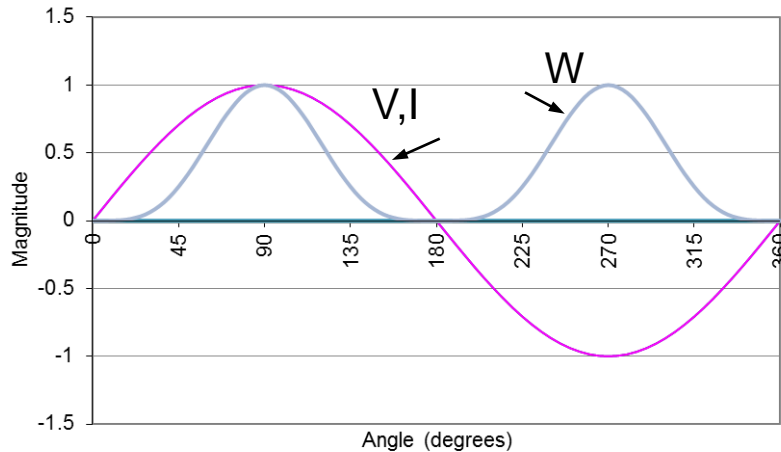
- Voltage drop is $\Delta\%$ of MVA values

$$\frac{8.1 - 0.6}{8.1} = 92.59\%$$

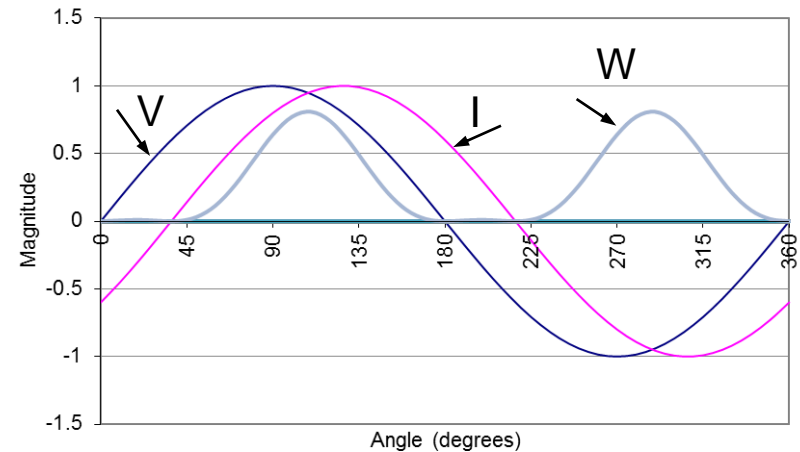
$$1 - 0.012 = 92.59\%$$



Power Factor



100% (unity) Power Factor

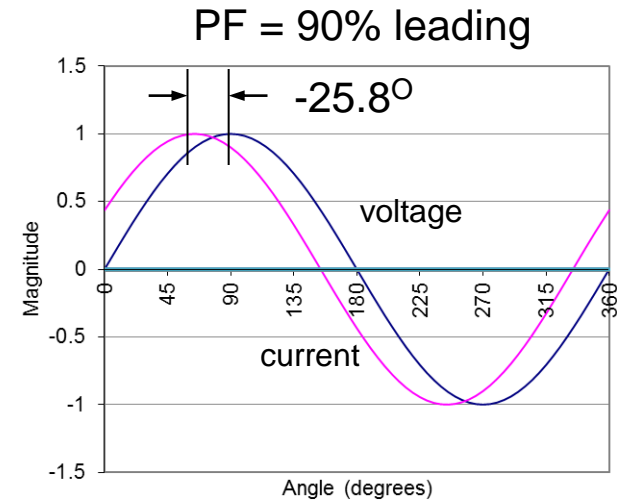
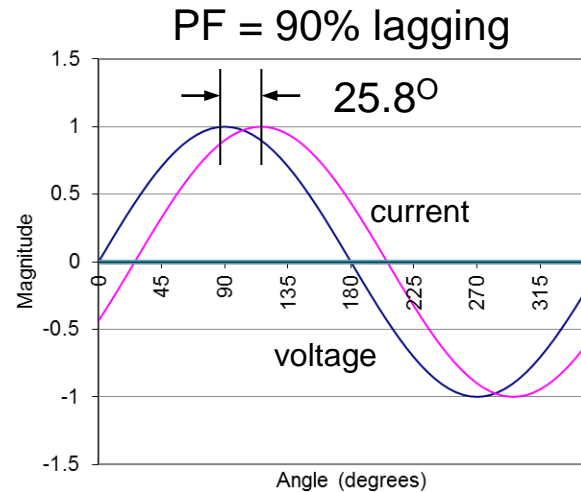
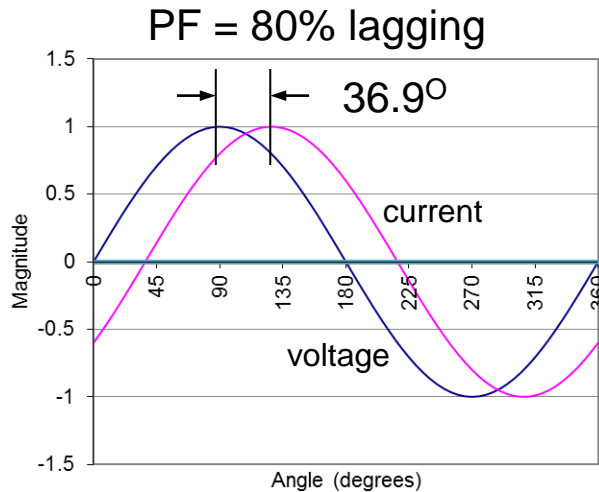
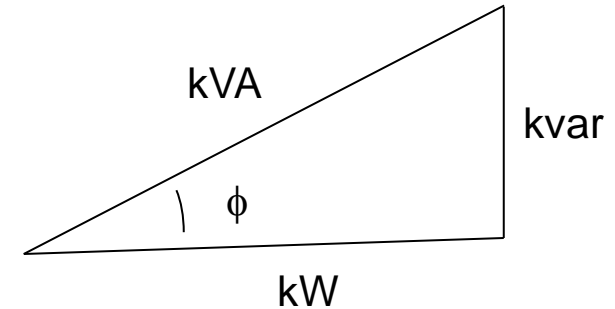


80% Power Factor
Less Watts, Same Current

- “Reactive” loads store and return energy each cycle
- Since they don’t “keep” the energy they consume, (ideally) there are no watts

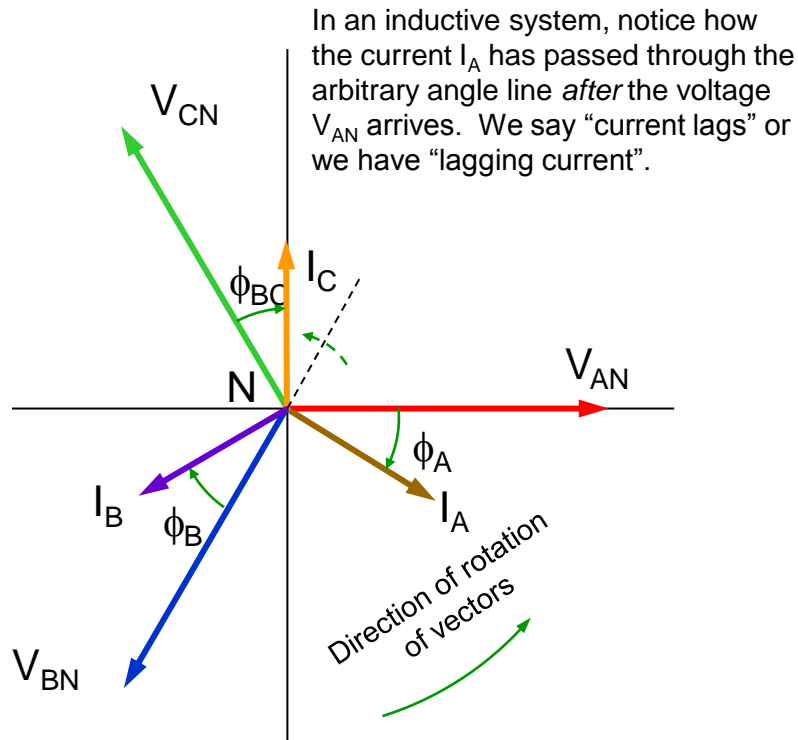
Power Factor

- $kVA = kV * I * \sqrt{3}$
- $\cos \theta = PF = \frac{kW}{kVA}$
- $\sin \theta = \frac{kvar}{kVA}$
- $kW = kVA \cos \theta = kVA * PF$

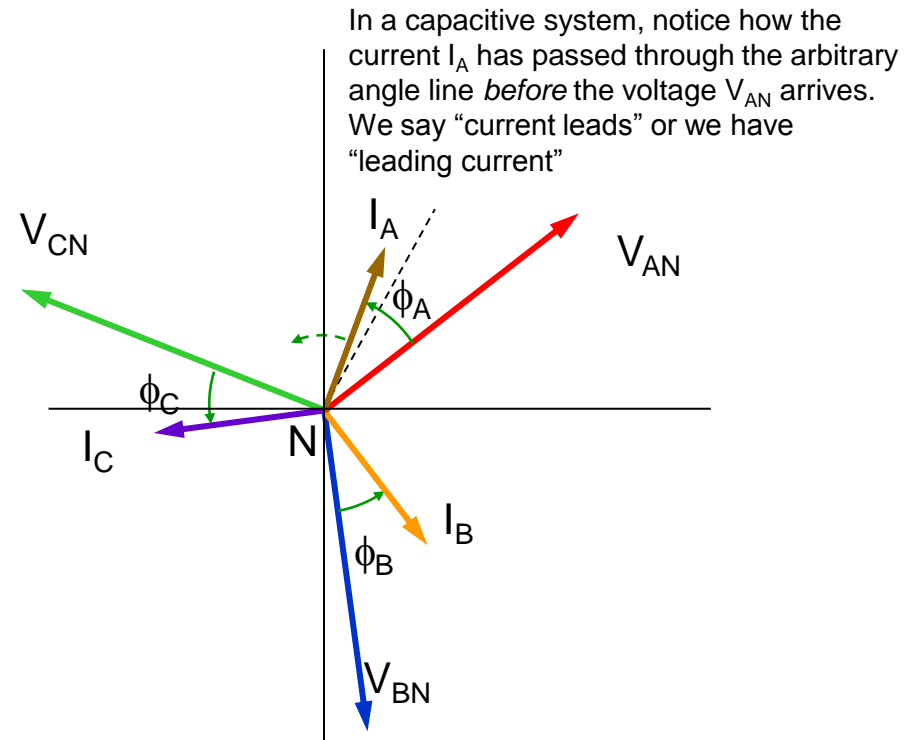


Power Factor Phasor Diagrams

Inductive System



Capacitive System



PF Rules of Thumb

- Use 35.0-11 to size motor capacitors
- $\%CurrentReduction = 100 - 100 \left(\frac{PF_{orig}}{PF_{new}} \right)$
- $ActualVars = NameplateVars * \frac{AppliedVoltage^2}{NameplateVoltage^2}$
- $\%VoltageRise = \frac{MVA_{cap}}{MVA_{SC}}$
 - MVA_{cap} : rating of capacitors added
 - MVA_{SC} : system short circuit capacity

More RoTs: Capacitance vs vars

- $kvar = kV * I_{cap}$
- $X_{cap} = \frac{1}{j2\pi fC}$
- $V = I * X_{cap} = I * \frac{1}{j2\pi fC}$
- $C = \frac{I}{2\pi f * kV} = \frac{kvar}{2\pi f * kV^2}$
- $var = 2\pi fC * V^2$
 - Note that the $kvar$ varies by the square of the voltage
 - Same capacitance will have many more vars at higher voltages

But don't just install a capacitor...

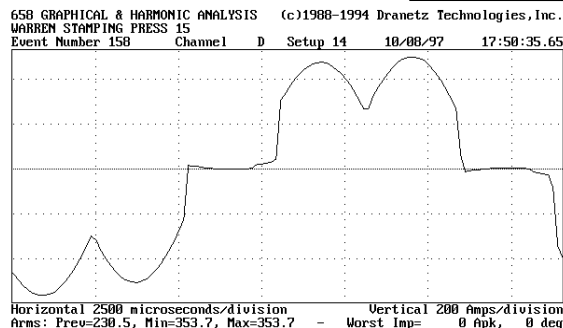
- Applying PF Correction Capacitors

- Utility penalties for low PF
- Pressure to reduce operating costs
- Capacity issues

$$HN = \sqrt{\frac{kVA / \%Z}{kvar}}$$

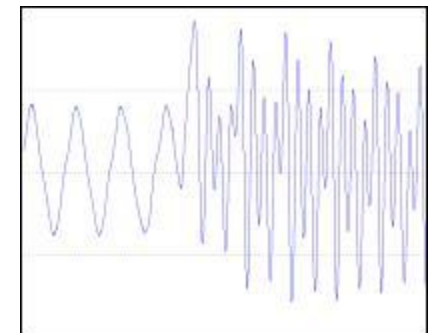
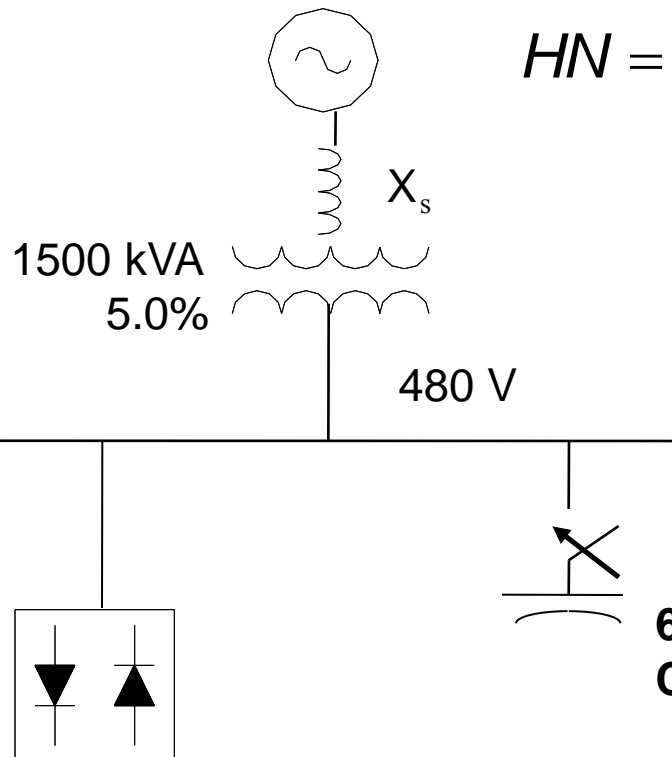
$$HN = \sqrt{\frac{1500 / 0.05}{600}} = 7.07$$

**200 kVA Drive/UPS
Source of
Harmonics**



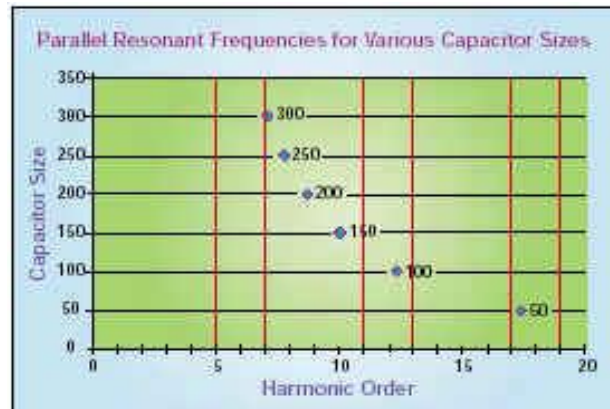
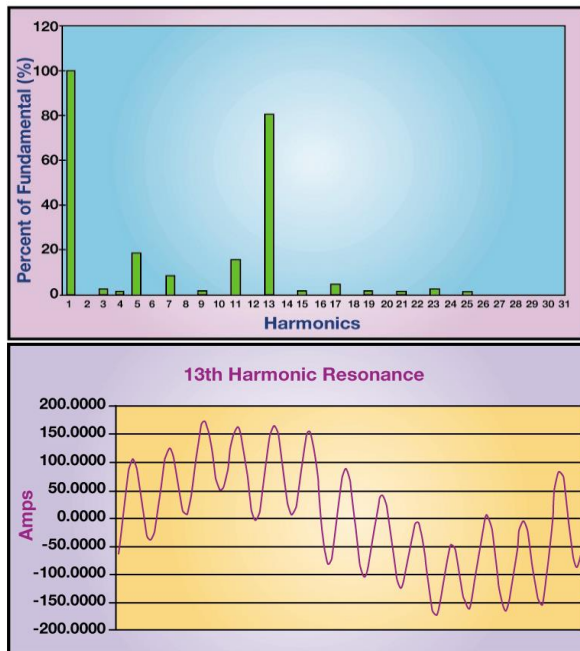
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Harmonic Resonance Solutions

- Apply another method of PF compensation (passive filter, active filter, etc)
- Eliminate harmonic source
- Change size of cap bank to over or under-compensate for required kvar and live with the ramifications.



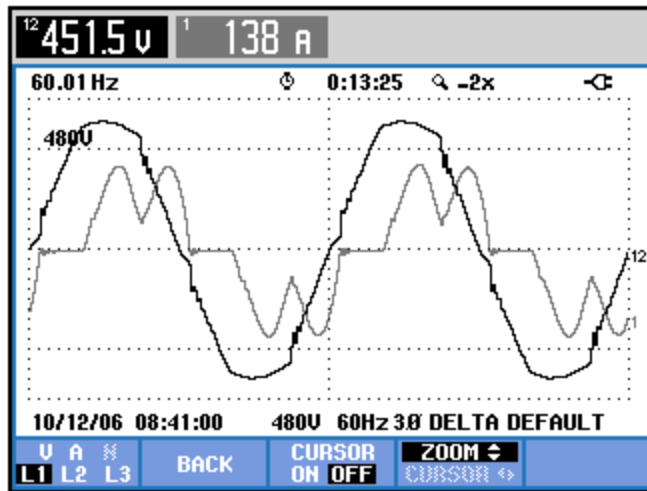
Note!
Every step of a switched capacitor bank must be checked to avoid parallel resonance

Problem gets worse with generators...

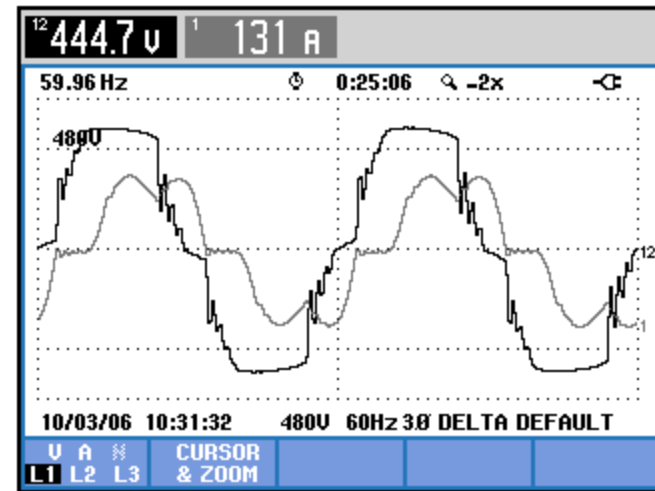
- Generator Concerns

- Generator impedance is generally 3-4 times (16-18%) the equivalent source transformer (5-6%)
- Harmonics can change even with the same load

$$HN = \sqrt{\frac{kVA / \%Z}{kvar}}$$

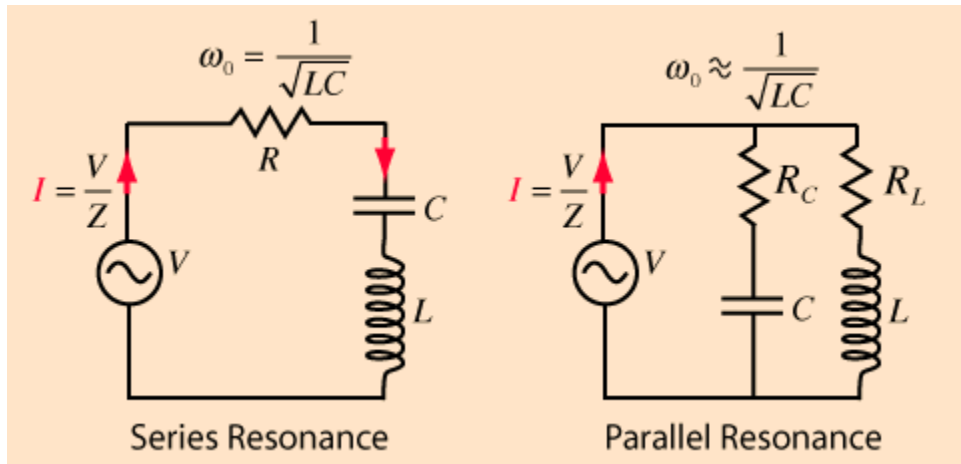


Utility Source
4.4% Vthd



Generator Source
13% Vthd

Wiring to Capacitor Matters



$$\omega_0 = \frac{1}{\sqrt{LC}} \left[\frac{R_L^2 C - L}{R_C^2 C - L} \right]^{\frac{1}{2}}$$

- If R_C greater than 0 (always will be):
 - Capacitive reactance factor decreases with increasing R_C
 - Just like with SPD lead length, minimize capacitor lead length

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